## A Discrete-Time Differential Dynamic Programming Algorithm with Application to Optimal Orbit Transfer

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Recently, the notion of Differential Dynamic Programming has been used to obtain new second-order algorithms for solving nonlinear optimal control problems. (Unlike conventional Dynamic Programming, the Principle of Optimality is applied in the neighborhood of a nominal, nonoptimal, trajectory.) A novel feature of these algorithms is that they permit strong variations in the system trajectory. In this paper Differential Dynamic Programming is used to develop a second-order algorithm for solving discrete-time dynamic optimization problems with terminal constraints. This algorithm also utilizes strong variations and, as a result, has certain advantages over existing discrete-time methods. A nonlinear computed example is presented, and comparisons are made with the results of other researchers who have solved this problem. The experience gained during the computation has suggested some extensions to an earlier, previously published Differential Dynamic Programming algorithm for continuous time problems. These extensions, and their implications, are discussed.

#### Notation

THE scalar product of column vectors a and b, where

$$a = \begin{bmatrix} a_1 \\ \vdots \\ a_n \end{bmatrix} \qquad b = \begin{bmatrix} b_1 \\ \vdots \\ b_n \end{bmatrix}$$

is  $a^Tb$  or  $b^Ta$  and is equal to

$$\sum_{i=1}^{n} a_i b_i$$

The derivative of a scalar V by a column vector x is a row vector, and is written as

$$V_x = \partial V/\partial x = [\partial V/\partial x_1, \dots, \partial V/\partial x_n]$$

The second derivative of a scalar V by vectors x and k is a matrix

$$V_{xk} = \frac{\partial^2 V}{\partial x \partial k} = \begin{bmatrix} \frac{\partial^2 V}{\partial x_1 \partial k_1} & \cdots & \frac{\partial^2 V}{\partial x_1 \partial k_m} \\ \vdots & & \vdots \\ \frac{\partial^2 V}{\partial x_n \partial k_1} & \cdots & \frac{\partial^2 V}{\partial x_n \partial k_m} \end{bmatrix}$$

Received September 15, 1969; revision received February 16, 1970. The authors wish to thank A. E. Bryson Jr. for his valuable suggestions, and R. G. Tobey of IBM for the use of the FORMAC system, which was helpful in manipulation of the rather complicated algebraic expressions that appear in this paper. S. B. Gershwin wishes to thank D. H. Jacobson for his patience and accessibility during the preparation of this paper. The research reported in this document was made possible through support extended the Division of Engineering and Applied Physics, Harvard University by the U.S. Army Research Office, the U.S. Air Force Office of Scientific Research and the U.S. Office of Naval Research under the Joint Services Electronics Program by Contracts N00014-67-A-0298-0006, 0005, and 0008 and by NASA under Grant NGR 22-007-068.

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where x is an n vector and k is an m vector. A second-order Taylor expansion is written as

$$V(x + \delta x, k + \delta k) = V(x, k) + V_x \delta x + V_k \delta k + \frac{1}{2} \delta x^T V_{xx} \delta x + \delta x^T V_{xk} \delta k + \frac{1}{2} \delta k^T V_{kk} \delta k$$

#### I. Introduction

Jacobson<sup>1-3</sup> has derived a second-order algorithm for solving continuous time optimal control problems using Differential Dynamic Programming. This algorithm differs from other second-order or second-variation algorithms<sup>4-11</sup> in that it is derived using global variations in control (strong variations in the trajectory).‡

In this paper a similar algorithm is developed for solving discrete-time dynamic optimization problems with terminal constraints. The new algorithm uses the notion of strong variations and hence, as in the case of the continuous time algorithm, has advantages over existing discrete-time algorithms.<sup>4,5,8,11</sup> The algorithm can be used to solve continuous time problems that are approximated by difference equations.

A nonlinear numerical example is presented and comparisons are drawn with McReynolds<sup>4,5</sup> and others<sup>7,12</sup> who have solved this problem previously, using other methods. The experience gained in the numerical computation has suggested extensions to the continuous algorithms in Refs. 1 and 2. In particular, the "step-size adjustment" technique is generalized by the introduction of additional criteria for ensuring that the "trial new trajectory," at each iteration, is sufficiently close to the current nominal trajectory to guarantee an improvement in cost and/or terminal error.

#### II. Derivation of the Discrete Algorithm

#### 1. Statement of the General Problem

The problem to be solved is the following: if  $x_0, \ldots, x_N$  are vector quantities which satisfy

$$x_{i+1} = f(x_i, u_i, t_i) \tag{1}$$

<sup>‡</sup> Although global variations in control are used, only small changes are allowed in the trajectory. Thus the method is not one for finding global minima. However, convergence to a local minimum is usually faster than that obtainable using existing "weak variation algorithms."

and  $x_o$  is given, find the vectors  $u_o, \ldots, u_{N-1}$  to minimize the scalar

$$\hat{W} = \sum_{i=0}^{N-1} L(x_i, u_i, t_i) + F(x_N)$$
 (2)

where the solution must satisfy the (vector) equality constraint

$$\theta(x_N) = 0 \tag{3}$$

N and  $t_o, \ldots, t_N$  are known quantities, and a nominal control  $\bar{u}_o, \ldots, \bar{u}_{N-1}$  is assumed given.

The minimized value of  $\hat{W}$  is referred to as  $\hat{V}$ . Defining

$$W(x_o, k, t_o) = \hat{W} + k^T \theta \tag{4}$$

the equivalent problem of finding  $u_o, \ldots, u_{N-1}$  to minimize  $W(x_o, k, t_o)$ § and k to satisfy Eq. (3) is solved in the following sections. A nominal value of k,  $\bar{k}$ , is assumed given.

The minimized value of  $W(x_o, k, t_o)$  is referred to as  $V(x_o, k, t_o)$ . More generally, if

$$W(x_{i},k,t_{i}) = \sum_{i=j}^{N-1} L(x_{i},u_{i},t_{i}) + F(x_{N}) + k^{T}\theta(x_{N})$$

where  $x_{j+1}, \ldots, x_N, u_j, \ldots, u_{N-1}$  satisfy (1), then

$$V(x_j,k,t_i) = \min_{u_i,i \ge j} W(x_j,k,t_j)$$

and V is called the optimal return function.

The nominal trajectory  $\bar{x}_o = x_o, \bar{x}_1, \ldots, \bar{x}_N$  is the solution to (1) with  $u_i = \bar{u}_i, i = 0, \ldots, N-1$ . The nominal return function  $\bar{W}(\bar{x}_i,\bar{k},t_i)$  is evaluated with  $k=\bar{k}$  along the nominal trajectory.

#### 2. Outline of the Solution

The optimal return function V satisfies Bellman's "Principle of Optimality," which in this case is

$$V(x_{i},k,t_{i}) = \min_{i} [L(x_{i},u_{i},t_{i}) + V(x_{i+1},k,t_{i+1})]$$
 (5)

for  $i = 0, \ldots, N-1$ .

Regarded in terms of displacement  $\delta x_i$ ,  $\delta x_{i+1}$ , and  $\delta k$  from the nominal trajectory,

$$x_i = \bar{x}_i + \delta x_i, x_{i+1} = \bar{x}_{i+1} + \delta x_{i+1}, k = \bar{k} + \delta k$$

and Eq. (5) becomes

$$V(\bar{x}_{i} + \delta x_{i}, \bar{k} + \delta k, t_{i}) = \min_{u_{i}} [L(\bar{x}_{i} + \delta x_{i}, u_{i}, t_{i}) + V(\bar{x}_{i+1} + \delta x_{i+1}, \bar{k} + \delta k, t_{i+1})]$$
(6)

The algorithm is derived from Eq. (6) in the following sequence of steps:

- 1) Expand both sides in Taylor series¶ about  $\bar{x}_i$ ,  $\bar{k}$  and  $\bar{x}_{i+1}$  in  $\delta x_i$ ,  $\delta k$ , and  $\delta x_{i+1}$ .
  - 2) Relate  $\delta x_{i+1}$  to  $\delta x_i$ .
- 3) Perform the indicated minimization with respect to  $u_i$  in two stages.
- a) Find  $u^{i*}$  which minimizes the right side of Eq. (6) with  $\delta x_i = 0$  and  $\delta k = 0.**$

¶ In some problems, typically continuous time, bang-bang with terminal constraints,  $\partial V(x_i,k_it_i)/\partial x$  and  $\partial^2(x_i,k_it_i)/\partial x^2$  are not continuous throughout the state space. Reference 3 extends Differential Dynamic Programming to that class of problems.

\*\* The min H approach of Kelley et al. 14 is similar to this step.

- b) Expand about  $u_i^*$  with  $\delta x_i$  and  $\delta k$  nonzero, and minimize with respect to  $\delta u_i$ . This gives  $\delta u_i$  as a function of  $\delta x_i$  and  $\delta k$ .
- 4) Equate coefficients of like powers of  $\delta x_i$  and  $\delta k$  to obtain difference equations in  $V_{x^i}$ ,  $V_{k^i}$ , etc.

It is assumed that  $\delta x_i$ ,  $\delta x_{i+1}$ , and  $\delta k$  are sufficiently small so that all Taylor expansions can be terminated at second-order terms.

#### 3. Solution

Following the prescription of the previous section, the left side of Eq. (6), when expanded in a Taylor series, is

$$V(\bar{x}_{i} + \delta x_{i},\bar{k} + \delta k,t_{i}) = V(\bar{x}_{i},\bar{k},t_{i}) + (\partial/\partial x)V(\bar{x}_{i},\bar{k},t_{i})\delta x_{i} + (\partial/\partial k)V(\bar{x}_{i},\bar{k},t_{i})\delta k + \frac{1}{2}\delta x_{i}^{T}(\partial^{2}/\partial x^{2})V(\bar{x}_{i},\bar{k},t_{i})\delta x_{i} + \delta x_{i}^{T}(\partial^{2}/\partial x\partial k)V(\bar{x}_{i},\bar{k},t_{i})\delta k + \frac{1}{2}\delta k^{T}(\partial^{2}/\partial k^{2})V(\bar{x}_{i},\bar{k},t_{i})\delta k + \dots$$
(7)

The reader should note that  $V(\bar{x}_i,\bar{k},t_i)$  is the minimal value of the return function obtainable with initial conditions at  $\bar{x}_i$ ,  $t_i$ , and with  $k = \bar{k}$ . It is not the same as  $\overline{W}(\bar{x}_i,\bar{k},t_i)$ , the value of the return function calculated along the nominal trajectory, starting from  $t_i$ .

Symbolically,

$$V(\bar{x}_{i}, \bar{k}, t_{i}) = \min_{u_{i}, \dots, u_{N-1}} \times \left[ \sum_{j=i}^{N-1} L(x_{j}, u_{j}, t_{j}) + F(x_{N}) + \bar{k}^{T} \theta(x_{N}) \right]$$
(8)

where  $x_{i+1}, \ldots, x_N$  satisfy Eq. (1), and  $x_i = \bar{x}_i$ . However,

$$\overline{W}(\bar{x}_{i},\bar{k},t_{i}) = \sum_{j=i}^{N-1} L(\bar{x}_{j},\bar{u}_{j},t_{j}) + F(\bar{x}_{N}) + \bar{k}^{T}\theta(\bar{x}_{N})$$
(9)

where  $\bar{u}_{i_1}, \ldots, \bar{u}_{N-1}$  is the nominal control sequence and thus,  $\bar{x}_{i_1}, \ldots, \bar{x}_{N}$  is the nominal trajectory [which satisfies Eq. (1) with  $u_j = \bar{u}_j, j = i, \ldots, N-1$ ].

Acknowledging the difference between  $V(\bar{x}_i, \bar{k}, t_i)$  and  $\bar{W}(\bar{x}_i, \bar{k}, t_i)$ , we define

$$a(\bar{x}_i, \bar{k}, t_i) = V(\bar{x}_i, \bar{k}, t_i) - \overline{W}(\bar{x}_i, \bar{k}, t_i)$$
 (10)

To simplify notation, let

$$\begin{split} \overline{W}(\bar{x}_i, \bar{k}, t_i) &= \overline{W}^i, \ V(\bar{x}_i, \bar{k}, t_i) = V^i \\ a(\bar{x}_i, \bar{k}, t_i) &= a^i, \ (\partial/\partial x) V(\bar{x}_i, \bar{k}, t_i) = V_{x^i}, \ \text{etc.} \end{split}$$

Then

$$a^i = V^i - \overline{W}^i \tag{10'}$$

and using Eq. (10) in Eq. (7), we obtain

$$V(\bar{x}_i + \delta x_i, \bar{k} + \delta k, t_i) = a^i + \bar{W}^i + V_{x^i} \delta x_i + V_{k^i} \delta k + \frac{1}{2} \delta x^{iT} V_{xx^i} \delta x_i + \delta x_i^T V_{xk^i} \delta k + \frac{1}{2} \delta k^T V_{kk^i} \delta k + \dots$$

$$(11)$$

Similarly, expanding the quantity to be minimized in Eq. (6) about  $\bar{x}_i$ ,  $\bar{k}$ ,  $\bar{x}_{i+1}$ , †† we obtain

$$L^{i} + L_{x}^{i}\delta x_{i} + \frac{1}{2}\delta x_{i}^{T}L_{xx}^{i}\delta x_{i} + a^{i+1} + \overline{W}^{i+1} + V_{x}^{i+1}\delta x_{i+1} + V_{k}^{i+1}\delta k + \frac{1}{2}\delta x_{i+1}^{T}V_{xx}^{i+1}\delta x_{i+1} + \delta x_{i+1}^{T}V_{xk}^{i+1}\delta k + \frac{1}{2}\delta k^{T}V_{kk}^{i+1}\delta k + \dots$$
(12)

where, as above,  $a^{i+1} + \bar{W}^{i+1} = V^{i+1}$ 

<sup>§</sup> It is well known that Eq. (4) need only have a stationary point with respect to u, for fixed k for the original problem to have a solution. Here, attention is restricted to that class of problems where Eq. (4) has a minimum with respect to u, for fixed k. Problems not belonging to this class may be handled by other techniques; for example, the penalty function method of Kelley.<sup>12</sup>

<sup>††</sup> L and its derivatives are evaluated at  $\bar{x}_{i}, u_{i}, t_{i}$ . The control  $u_{i}$  is yet to be determined.

Expression (12) is an infinite series in  $\delta x_i$ ,  $\delta x_{i+1}$ , and  $\delta k$ ; however, it is clear that there is a relationship between  $\delta x_i$  and  $\delta x_{i+1}$  through Eq. (1). This relationship may be used to eliminate either  $\delta x_i$  or  $\delta x_{i+1}$  from (12), but to conform with Eq. (11),  $\delta x_{i+1}$  is removed. Using the following equations:

$$x_{i+1} = f(x_i, u_i, t_i), \ \bar{x}_{i+1} = f(\bar{x}_i, \bar{u}_i, t_i)$$

we obtain

$$\delta x_{i+1} = f(x_i, u_i, t_i) - f(\bar{x}_i, \bar{u}_i, t_i)$$

or,

$$\delta x_{i+1} = f(\bar{x}_i + \delta x_i, u_i, t_i) - f(\bar{x}_i, \bar{u}_i, t_i)$$
 (13)

In Eq. (13),  $u_i$  is perfectly general. It is chosen later by the minimization operation of Eq. (6). Expanding Eq. (13) about  $\bar{x}_i$ , and defining

$$f^i = f(\bar{x}_i, u_i, t_i), \bar{f}^i = f(\bar{x}_i, \bar{u}_i, t_i)$$

we obtain

$$\delta x_{i+1} = (f^i - \tilde{f}^i) + f_x i \delta x_i + \frac{1}{2} \delta x_i^T f_{xx} i \delta x_i + \dots$$
 (14)

where the derivatives of  $f^i$  are evaluated at  $(\bar{x}_i, u_i, t_i)$ . Substituting Eq. (14) into Eq. (12), we obtain

$$L^{i} + a^{i+1} + \overline{W}^{i+1} + V_{x^{i+1}}(f^{i} - \overline{f}^{i}) + \frac{1}{2}(f^{i} - \overline{f}^{i})^{T}V_{xx^{i+1}}(f^{i} - \overline{f}^{i}) + [L_{x^{i}} + V_{x^{i+1}}f_{x^{i}} + f_{x^{i}}^{T}V_{xx^{i+1}}(f^{i} - \overline{f}^{i})]\delta x_{i} + [V_{k^{i+1}} + (f^{i} - \overline{f}^{i})^{T}V_{xk^{i+1}}]\delta k + \delta x_{i}^{T}f_{x^{i}}V_{xk^{i+1}}\delta k + \frac{1}{2}\delta k^{T}V_{kk^{i+1}}\delta k + \frac{1}{2}\delta x_{i}^{T}[L_{xx^{i}} + V_{x^{i+1}}f_{xx^{i}} + f_{x^{i}}^{T}V_{xx^{i+1}}f_{x^{i}} + (f^{i} - \overline{f}^{i})^{T}V_{xx^{i+1}}f_{xx^{i}}]\delta x_{i} + \dots$$

$$(15)$$

Clearly Eq. (5) has now been transformed to:

right-hand side of Eq. (11) = 
$$\min_{u_i} \{ \text{expression (15)} \}$$
 (16)

As suggested earlier, the minimization in Eq. (16) is performed in two stages.

First,  $u_i^*$  is found which minimizes expression (15) with  $\delta x_i = 0$  and  $\delta k = 0$ , i.e.,  $u_i^*$  minimizes

$$L^{i} + a^{i+1} + \bar{W}^{i+1} + V_{x}^{i+1}(f^{i} - \bar{f}^{i}) + \frac{1}{2}(f^{i} - \bar{f}^{i})^{T}V_{xx}^{i+1}(f^{i} - \bar{f}^{i}) + \dots$$
 (17)

[The terms not printed in expression (17) are of third and higher order in  $(f^i - \bar{f}^i)$ , and are assumed to be negligible.]

For convenience, we define

$$H^{i} = H(\bar{x}_{i}, u_{i}^{*}, \bar{k}, t_{i}) = L^{i} + V_{x}^{i+1} f^{i}$$
(18)

In Eq. (18), and for the rest of this paper, all functions of  $u_i$ , other than  $\bar{f}^i$ , are evaluated at  $u_i^*$ .

Note that

$$H_{x^i} = L_{x^i} + V_{x^{i+1}} f_{x^i}$$

$$H_{xx^i} = L_{xx^i} + V_{x^{i+1}} f_{xx^i}$$
, etc.

Since expression (17) is at a minimum when evaluated at  $u_i^*$ , its first derivative with respect to  $u_i$  must be zero

$$H_{u}^{i} + (f^{i} - \bar{f}^{i})^{T} V_{xx}^{i+1} f_{u}^{i} = 0 \tag{19}$$

In addition, the second derivative of expression (17) (defined as  $\Delta$ ) must be positive definite at  $u_i = u_i^*$ ;

$$\Delta = H_{uu}^{i} + f_{u}^{iT}V_{xx}^{i+1}f_{u}^{i} + (f^{i} - \bar{f}^{i})^{T}V_{xx}^{i+1}f_{uu}^{i} > 0 \quad (20)$$

[The third term in Eq. (20) does not appear in the "weak variation" algorithms of Refs. 4, 5, 8, and 11].

Expanding expression (15) about  $u_i^*$ , with  $u_i = u_i^* + \delta u_i$ , the following is obtained, using Eqs. (19) and (20):

$$\begin{split} L^{i} + a^{i+1} + \overline{W}^{i+1} + V_{x}^{i+1}(f^{i} - \overline{f}^{i}) + \\ \frac{1}{2}(f^{i} - \overline{f}^{i})^{T}V_{xx}^{i+1}(f^{i} - \overline{f}^{i}) + [H_{x}^{i} + f_{x}^{iT}V_{xx}^{i+1}(f^{i} - \overline{f}^{i})]\delta x_{i} + [V_{k}^{i+1} + (f^{i} - \overline{f}^{i})^{T}V_{xk}^{i+1}]\delta k + \\ \delta x_{i}^{T}f_{x}^{iT}V_{xk}^{i+1}\delta k + \delta u_{i}^{T}f_{u}^{iT}V_{xk}^{i+1}\delta k + \delta x_{i}^{T}[H_{xu}^{i} + f_{x}^{iT}V_{xx}^{i+1}f_{u}^{i} + (f^{i} - \overline{f}^{i})^{T}V_{xx}^{i+1}f_{xu}^{i}]\delta u_{i} + \\ \frac{1}{2}\delta x_{i}^{T}[H_{xx}^{i} + f_{x}^{iT}V_{xx}^{i+1}f_{x}^{i} + (f^{i} - \overline{f}^{i})^{T}V_{xx}^{i+1}f_{xx}^{i}]\delta x_{i} + \\ \frac{1}{2}\delta k^{T}V_{kk}^{i+1}\delta k + \frac{1}{2}\delta u_{i}^{T}\Delta \delta u_{i} \quad (21) \end{split}$$

Terms of order  $(\delta x_i)^3$ ,  $(\delta u_i)^3$ ,  $(\delta k)^3$  or greater have been ignored in expression (21).‡‡

The second stage of the minimization is accomplished when expression (21) is minimized with respect to  $\delta u_i$ . Taking the first derivative of expression (21) with respect to  $\delta u_i$  and setting it to zero, we obtain

$$\delta u_i = \beta_1 \delta x_i + \beta_2 \delta k \tag{22}$$

where

$$\beta_1 = -\Delta^{-1} [H_{ux}^i + f_{u}^{iT} V_{xx}^{i+1} f_{x}^i + (f^i - \bar{f}^i)^T V_{xx}^{i+1} f_{ux}^i]$$
(23)

$$\beta_2 = -\Delta^{-1} f_u^{iT} V_{xk}^{i+1} \tag{24}$$

Equation (22) is a linear feedback perturbation control law. It is sufficient to consider  $\delta u_i$  to be linear in  $\delta x_i$  and  $\delta k$  because on substituting an expression of higher order than (22) into (21), terms of higher order than quadratic would appear.

On substituting Eq. (22) into expression (21), we obtain

$$\begin{array}{c} L^{i}+a^{i+1}+\overline{W}^{i+1}+V_{x}^{i+1}(f^{i}-\overline{f}^{i})+\\ \frac{1}{2}(f^{i}-\overline{f}^{i})^{T}V_{xx}^{i+1}(f^{i}-\overline{f}^{i})+[H_{x}^{i}+(f^{i}-\overline{f}^{i})+[H_{x}^{i}+(f^{i}-\overline{f}^{i})^{T}V_{xx}^{i+1}]\delta k+\\ \overline{f}^{i})^{T}V_{xx}^{i+1}f_{x}^{i}]\delta x_{i}+[V_{k}^{i+1}+(f^{i}-\overline{f}^{i})^{T}V_{xk}^{i+1}]\delta k+\\ \delta x_{i}^{T}[f_{x}^{iT}V_{xk}^{i+1}-\beta_{1}^{T}\Delta\beta_{2}]\delta k+\frac{1}{2}\delta x_{i}^{T}[H_{xx}^{i}+f_{x}^{i}+(f^{i}-\overline{f}^{i})V_{xx}^{i+1}f_{xx}^{i}-\beta_{1}^{T}\Delta\beta_{1}]\delta x_{i}+\\ \frac{1}{2}\delta k^{T}[V_{kk}^{i+1}-\beta_{2}^{T}\Delta\beta_{2}]\delta k \end{array}$$

Expression (25) is the minimum of (15) with respect to  $u_i$ . Thus, from Eq. (16), expression (25) is equal to the right-hand side of Eq. (11), so that coefficients of like powers of  $\delta x_i$  and  $\delta k$  are equal.

Noting that

$$\overline{W}^i = \overline{W}^{i+1} + \overline{L}^i \tag{26}$$

and equating (11) and (25) produces the following difference equations, valid for  $i = 0, \ldots, N-1$ :

$$a^{i} = a^{i+1} + H^{i} - H^{i} + \frac{1}{2}(f^{i} - \bar{f}^{i})^{T} V_{xx}^{i+1}(f^{i} - \bar{f}^{i})$$
 (27)

$$V_{x^{i}} = H_{x^{i}} + (f^{i} - \bar{f}^{i})^{T} V_{xx^{i+1}} f_{x^{i}}$$
(28)

$$V_{k}^{i} = V_{k}^{i+1} + (f^{i} - \bar{f}^{i})^{T} V_{xk}^{i+1}$$
(29)

$$V_{xk}^{i} = f_{x}^{iT} V_{xk}^{i+1} - \beta_{1}^{T} \Delta \beta_{2}$$
 (30)

$$V_{kk}^i = V_{kk}^{i+1} - \beta_2 \Delta \beta_2 \tag{31}$$

$$V_{xx^{i}} = H_{xx^{i}} + f_{x^{iT}}V_{xx^{i+1}}f_{x^{i}} + (f^{i} - \bar{f}^{i})V_{xx^{i+1}}f_{xx^{i}} - \beta_{1}^{T}\Delta\beta_{1}$$
(32)

The boundary conditions are applied at i = N, and are the same as in Refs. 1 and 2. They are found by expanding

$$V(\bar{x}_N + \delta x_N, \bar{k} + \delta k, t_N) = F(\bar{x}_N + \delta x_N) + (\bar{k} + \delta k)^T \theta(\bar{x}_N + \delta x_N)$$

<sup>‡‡</sup> It is assumed that  $\delta x_i$ ,  $\delta u_i$ , and  $\delta k$  are small enough to justify this truncation.

to second order in a Taylor series in  $\delta x_N$  and  $\delta k$ . Because this is the last time step  $\overline{W}^N = V^N$  so that

$$a^N = 0 (33)$$

and,

$$V_{x^N} = F_x(\bar{x}_N) + \bar{k}^T \theta_x(\bar{x}_N) \tag{34}$$

$$V_{k^N} = \theta^T(\bar{x}_N) \tag{35}$$

$$V_{xk}^{N} = \theta_x^{T}(\bar{x}_N) \tag{36}$$

$$V_{kk}^{N} = 0 (37)$$

$$V_{xx}^{N} = F_{xx}(\bar{x}_N) + \bar{k}^T \theta_{xx}(\bar{x}_N)$$
 (38)

Thus if we "integrate" Eqs. (27–32) from i = N - 1 to 0 with Eqs. (33–38) as boundary conditions, then Eqs. (19) and (22) show how to calculate  $u_i = u_i^* + \delta u_i$  to obtain optimal improvement in performance index  $V(x_o, k, t_o)$ .

These results are only meaningful if the second-order truncations of the Taylor series above are good approximations of the full expansions. Thus  $\delta x_i$ ,  $\delta x_{i+1}$ ,  $\delta k$ , and  $\delta u_i$  must be small. Note that there is no restriction on  $\Delta u_i = u_i^* - \bar{u}_i$  except that  $f^i - \bar{f}^i = f(\bar{x}_i, u_i^*, t_i) - f(\bar{x}_i, \bar{u}_i, t_i)$  must be sufficiently small to guarantee the smallness of  $\delta x_{i+1}$ .

## III. Comparison with and Extensions of Jacobson's Results

#### 1. Comparison and Discussion

The case in which the discrete problem is a Euler discretization of a continuous problem is of interest. In that case,

$$f(x_i, u_i, t_i) = x_i + \Delta t \tilde{f}(x_i, u_i, t_1) \tag{39}$$

and

$$L(x_i, u_i, t_i) = \tilde{L}(x_i, u_i, t_i) \Delta t \tag{40}$$

Clearly,

$$\dot{x}(t_i) = \lim_{\Delta t \to 0} \frac{x(t_i + \Delta t) - x(t_i)}{\Delta t} = \lim_{\Delta t \to 0} \frac{x_{i+1} - x_i}{\Delta t}$$
$$= \tilde{f}(x_i, u_i, t_i) \quad (41)$$

and

$$\lim_{\substack{\Delta t \to 0 \\ N \to \infty}} \sum_{i=0}^{N-1} L(x_i, u_i, t_i) = \lim_{\substack{\Delta t \to 0 \\ N \to \infty}} \sum_{i=0}^{N-1} \tilde{L}(x_i, u_i, t_i) \, \Delta t$$

$$= \int_{t_0}^{tN} \tilde{L} \left[ x(t), u(t), t \right] dt \quad (42)$$

if the discretization is done with care.

It is reasonable to expect that if transformations (39) and (40) are applied to the results of the previous section and the limit is taken as  $\Delta t \rightarrow 0$ , equations should be obtained which solve the analogous continuous problem. Jacobson<sup>1,2</sup> has solved that problem, and the statement and solution of the problem are reproduced in Appendix A.

Note that

$$H^{i} = \tilde{L}^{i} \Delta t + V_{x}^{i+1} (\bar{x}_{i} + \Delta t \tilde{f}^{i})$$

so that

$$H^{i} = (\tilde{L}^{i} + V_{x}^{i+1}\tilde{f}^{i})\Delta t + V_{x}^{i+1}\tilde{x}_{i} = \tilde{H}^{i}\Delta t + V_{x}^{i+1}\tilde{x}_{i}$$
 (43)

Then, according to Eq. (20)

$$\Delta = \tilde{H}_{uu}^{i} \Delta t + (\Delta t)^{2} [\tilde{f}_{u}^{i} V_{xx}^{i+1} \tilde{f}_{u}^{i} + (\tilde{f}^{i} - \tilde{f}^{i}) V_{xx}^{i+1} \tilde{f}_{uu}^{i}]$$
 (44)

Now define

$$\tilde{\Delta} = \Delta/\Delta t \tag{45}$$

which we write as

$$\tilde{\Delta} = \tilde{H}_{uu^i} + A^i \Delta t \tag{46}$$

for clarity.

From Eqs. (23) and (45),

$$\beta_{1} = -\tilde{\Delta}^{-1}(\tilde{H}_{ux}^{i} + \tilde{f}_{u}^{iT}V_{xx}^{i+1}) - \tilde{\Delta}^{-1}[\tilde{f}_{u}^{iT}V_{xx}^{i+1}\tilde{f}_{x}^{i+1} + (\tilde{f}^{i} - \overline{\tilde{f}}^{i})^{T}V_{xx}^{i+1}f_{ux}^{i}]\Delta t \quad (47)$$

Similarly, from Eq. (24),

$$\beta_2 = -\tilde{\Delta}^{-1} \tilde{f}_u^{iT} V_{xk}^{i+1} \tag{48}$$

In the same manner, applying Eqs. (39, 40, 43, 45, 47, and 48) to (27–32), the following equations are obtained:

$$-(a^{i+1} - a^{i})/\Delta t = \tilde{H}^{i} - \tilde{\bar{H}}^{i} + \frac{1}{2}(\tilde{f}^{i} - \tilde{\bar{f}}^{i})^{T}V_{xx}^{i+1}(\tilde{f}^{i} - \tilde{\bar{f}}^{i})\Delta t$$
(49)

$$-(V_{x^{i+1}} - V_{x^{i}})/\Delta t = \tilde{H}_{x^{i}} + (\tilde{f}^{i} - \bar{\tilde{f}}^{i})V_{xx^{i+1}} + (\tilde{f}^{i} - \bar{\tilde{f}}^{i})^{T}V_{xx^{i+1}}\tilde{f}_{x^{i}}\Delta t \quad (50)$$

$$-(V_{k^{i+1}} - V_{k^{i}})/\Delta t = (\tilde{f}^{i} - \tilde{f}^{i})^{T}V_{xk^{i+1}}$$
 (51)

$$-(V_{xk}^{i+1} - V_{xk}^{i})/\Delta t = \tilde{f}_x^{iT}V_{xk}^{i+1} - \beta_1^T \tilde{\Delta}\beta_2$$
 (52)

$$-(V_{kk}^{i+1} - V_{kk}^{i})/\Delta t = -\beta_2^T \tilde{\Delta}\beta_2$$
 (53)

$$\begin{split} -(V_{xx}^{i+1}-V_{xx}^{i})/\Delta t &= \tilde{H}_{xx}^{i} + \tilde{f}_{x}^{i} V_{xx}^{i+1} + V_{xx}^{i+1} \tilde{f}_{x}^{i} + \\ \beta_{1}{}^{T} \tilde{\Delta} \beta_{1} &+ \Delta t \left[ \tilde{f}_{x}^{i} V_{xx}^{i+1} \tilde{f}_{x}^{i} + (\tilde{f}^{i} - \tilde{f}^{i})^{T} V_{xx}^{i+1} \tilde{f}_{xx}^{i} \right] \end{split}$$
(54)

Jacobson's equations for  $\beta_1$ ,  $\beta_2$ , a,  $V_x$ ,  $V_k$ ,  $V_{xk}$ ,  $V_{kk}$ , and  $V_{xx}$  are reproduced in Appendix A. Inspection will reveal agreement between those and Eqs. (47–54) as  $\Delta t \rightarrow 0$ .

It should be noted that although the discrete f, L, and H are related to their respective continuous counterparts through Eqs. (39, 40, and 43), the discrete a,  $\overline{W}$ , derivatives of V,  $\beta_1$ , and  $\beta_2$  directly approximate the continuous quantities. As $\Delta t \to 0$ , the discrete and continuous versions of the latter quantities approach one another.

Equations (39) and (40) and the transformations that resulted from them have been used previously to show the connection between the present discrete equations and the earlier<sup>1,2</sup> continuous equations. However, cases may exist where Eqs. (39) and (40) are useful numerical methods with which to solve a continuous problem.§§ Then, Eqs. (47–54) contain the full dependence on  $\Delta t$ , which involves terms of order  $\Delta t$  and higher. It may be worthwhile to retain high-order terms.<sup>11</sup> Also, Eqs. (47–54) indicate that some of the arguments of the right sides are evaluated at time i + 1, and others are evaluated at time i. A simple Euler discretization of the continuous time algorithm would evaluate all arguments at time i + 1.

It may be possible to obtain more useful versions of Eqs. (47-54) by replacing Eq. (39) and Eq. (40), the Euler discretizations of f and L, by a more sophisticated, accurate scheme.

#### 2. Description of the Algorithm

The discrete algorithm is very similar to the continuous algorithm and is outlined in Fig. 1. The algorithm is a successive approximation process, and each approximation has two stages. In the first stage, k is kept constant, and optimization takes place with respect to  $u_i$ , without regard to the value of  $\theta$ . In the second,  $\delta k$  is calculated to reduce  $\theta$  in absolute value.

<sup>§§</sup> Continuous-time problems which are particularly sensitive to u may require a large number of small time steps when the algorithms of Refs. 1 and 2 are used. Then, since  $\Delta t$  is small, sufficient integration accuracy may be obtained from an Euler scheme.

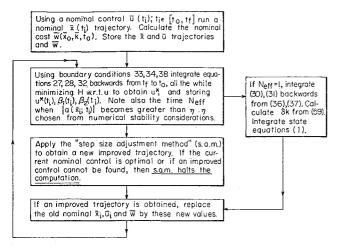


Fig. 1 Over-all computational procedure.

The first stage proceeds as follows. Equation (1) is "integrated" using initial conditions  $x_o$  and nominal control  $\bar{\mu}_0, \ldots, \bar{u}_{N-1}$ . Then Eqs. (27, 28, and 32) are integrated back from i=N, with boundary conditions (33, 34, and 38). If  $a^o$  is not close to zero, then, by definition (10), the nominal control is not close to optimal for the current value of  $\bar{k}$ . To improve the trajectory (i.e., to get closer to the optimal and reduce  $a^o$ ), Eq. (19) is solved for  $u_i^*$  and Eq. (22) is used to calculate  $u_i = u_i^* + \delta u_i$ , which is used as the new optimal control in Eq. (1). The cycle repeats. If necessary (see below for the descriptions of the tests to explain this necessity) the stepsize adjustment routine is called. For a complete description of this routine, see Appendix B and Ref. 2.

If  $a^o$  is close to zero, and  $\theta$  is also close to zero, the problem is solved. If  $a^o$  is close to zero but  $\theta$  is not, the algorithm enters its second stage: k is modified (according to the formula of the next section) to reduce each component of  $\theta$  in absolute value.

#### 3. Determination of $\delta k$

Jacobson has shown (Ref. 1, Sec. 2.3) that, to second order, the proper value of  $\delta k$  is that which maximizes  $V(\bar{x}_o, \bar{k} + \delta k, t_o)$ . ¶¶ We have

$$V(\bar{x}_0,\bar{k}+\delta k,t_0) = a^o + \bar{W}^o + V_{k^o} \delta k + \frac{1}{2} \delta k^T V_{kk^o} \delta k \quad (55)$$

so that the proper value of  $\delta k$  satisfies

$$V_{k^{0T}} + V_{kk^{o}}\delta k = 0 (56)$$

or

$$\delta k^T = -V_{kk^0}^{-1} V_{k^0}^T \tag{57}$$

(Jacobson shows that  $V_{kk^0}$  is negative definite,\* so that  $V_{kk^{0-1}}$  exists.)

Since, in the present algorithm,  $\delta k$  is only evaluated when  $f^i - \bar{f}^i = 0$  (because  $a^o = 0$ ),  $V_{k^o} = \theta^T(\bar{x}_N)$  from Eqs. (29) and (35). Thus, Eq. (57) becomes

$$\delta k = -V_{kk}^{o-1}\theta(\bar{x}_N) \tag{58}$$

Following Jacobson,  $^1k$  is modified according to Eq. (58); Eq. (1) is then integrated forward with  $u_i = u_i^* + \delta u_i$  chosen according to Eq. (19) and (22). If the resultant value of  $\theta(x_N)$  is not smaller in absolute value (component-wise) than  $\theta(\bar{x}_N)$ , choose

$$\delta k = -\epsilon V_{kk}^{o-1} \theta(\bar{x}_N) \tag{59}$$

where  $0 < \epsilon \le 1$ , and reduce  $\epsilon$  until  $\theta(x_N)$  is reduced and  $a^{\circ}$  is near zero.

#### 4. New Criteria

It is essential that  $\delta x_i$  and  $\delta k$  be kept small. This ensures that  $\delta u_i$  is small, and thus that the second-order expansions of Eq. (6) remain valid. If  $\delta x_i$  and  $\delta k$  are found to be too large, i.e., if they invalidate the truncations of the Taylor series in Sec. II, they should be reduced by Jacobson's techniques which apply to the discrete problem as well as to the continuous.

An additional criterion, required for fixed end point problems is described below (test 1). A criterion, alternative to that in Refs. 1 and 2, is also given. This criterion (test 2) is useful in cases where it is desirable to keep the new trajectory in the immediate neighborhood of the nominal.†

#### Test 1

Although  $\delta k$  is chosen according to Eq. (59) (where  $\epsilon$  is such that  $\theta(x_N)$  is reduced), it may lie outside the range of validity of the expansion Eq. (11) (when truncated at second-order terms).

At i=0, Eq. (11) coincides with Eq. (55). Since both sides of Eq. (55) may be independently measured, choose  $\delta k$  and evaluate the left-hand side. Then integrate Eq. (1) as described above and evaluate the right-hand side,  $V(\bar{x}_o, \bar{k} + \delta k, t_o)$ ; Eq. (55) may be considered to be a test of  $\delta k$ .

If  $\delta k$  is given by Eq. (59), then Eq. (55) predicts that

$$V(\bar{x}_o, \bar{k} + \delta k, t_o) - \bar{W}^o = a^o - (\epsilon - \frac{1}{2} \epsilon^2) \theta^T(\bar{x}_N) V_{kk}^{o-1} \theta(\bar{x}_N)$$
 (60)

If Eq. (60) does not predict the change in W to within a given tolerance,  $\epsilon$  should be reduced until it does.

#### Test 2

From Eqs. (4) and (9),

$$V^{i} = \sum_{j=i}^{N} L^{j} + F(x_{N}) + k^{T}\theta(x_{N})$$
 (61)

$$\overline{W}^{i} = \sum_{j=i}^{N} \bar{L}^{j} + F(\bar{x}_{N}) + \bar{k}^{T}\theta(\bar{x}_{N})$$
 (62)

Thus

$$\delta V^{i} = V^{i} - \overline{W}^{i} = \sum_{j=i}^{N} \delta L^{j} + [F(x_{N}) - F(\bar{x}_{N})] + [k^{T}\theta(x_{N}) - \bar{k}^{T}\theta(\bar{x}_{N})]$$
(63)

But, from Eq. (11),

$$\delta V^{i} = a^{i} + V_{x}^{i} \delta x_{i} + V_{k}^{i} \delta k + \frac{1}{2} \delta x_{i}^{T} V_{xx}^{i} \delta x_{i} + \delta x_{i}^{T} V_{xk}^{i} \delta k + \frac{1}{2} \delta k^{T} V_{kk}^{i} \delta k$$
(64)

Since Eqs. (63) and (64) are theoretically equal, their difference is a test of the size of  $\delta x_i$  and  $\delta k$ ; this is because Eq. (63) is an exact expression, and Eq. (64) is an approximation, correct to second-order terms.

In order to use Eqs. (63) and (64) as a step-by-step test of  $\delta x_i$ , their form should be modified. This is because Eq. (63) involves  $x_N$ , which is not available at step i of the forward integration. The modification is a simple one: from Eq. (63),

$$\delta V^{o} = \sum_{j=0}^{N} \delta L^{j} + [F(x_{N}) - F(\bar{x}_{N})] + [k^{T}\theta(x_{N}) - \bar{k}^{T}\theta(\bar{x}_{N})]$$
(65)

 $<sup>\</sup>P\P$  McReynolds<sup>4</sup> and Bryson and Ho<sup>15</sup> have obtained similar conditions.

<sup>\*</sup> Provided that the linearized system is controllable, and  $\theta_x^T$  has full rank.

<sup>†</sup> Such may be the case when the trajectory must be prevented from "jumping" to another nearby local minimum. In the following section, an example is discussed in detail where this was found to be necessary.

Table 1 100 time steps $-$ final t
------------------------------------

t	u	$x_1$	$x_2$	$x_3$	$V_{x_1}$	$V_{x_2}$	$V_{x3}$
0	0.4430	1	0	1	1.8890	0.94316	2.0604
0.166	0.5188	1.0008	0.0134	1.0201			
0.332	0.6073	1.0044	0.0353	1.0366	1.5777	0.94982	1.4229
0.498	0.7097	1.0121	0.0649	1.0478			
0.664	0.8269	1.0252	0.1011	1.0520	1.2963	0.85152	0.82311
0.830	0.9592	1.0446	0.1419	1.0479			
0.996	1.107	1.0711	0.1853	1.0349	1.0857	0.64554	0.34816
1.162	1.271	1.1047	0.2288	1.0129			
1.328	1.460	1.1455	0.2701	0.9823	0.96818	0.36222	0.055367
1.494	1.730	1.1929	0.3071	0.9433			
1.660	2.886	1.2459	0.3347	0.8924	0.93356	0.045050	-0.048480
1.826	4.493	1.3008	0.3157	0.8370			
1.992	4.765	1.3508	0.2786	0.8032	0.95639	-0.27469	0.0036793
2.158	4.913	1.3945	0.2390	0.7811			
2.324	5.023	1.4315	0.1991	0.7675	1.0117	-0.58597	0.17505
2.490	5.116	1.4619	0.1600	0.7611			
2.656	5.196	1.4860	0.1225	0.7609	1.1031	-0.88384	0.44689
2.822	5.269	1.5039	0.0872	0.7661			
2.988	5.335	1.5162	0.0546	0.7762	1.2105	-1.1608	0.81108
3.154	5.398	1.5233	0.0254	0.7908			
3.320		1.5257	0.0000	0.8096	1.3356	-1.4034	1.2647

 $^{a}V = 1.52572699, k_{1} = -1.40339248, k_{2} = 1.26501024, \theta_{1} = 0.75 \times 10^{-6}, \theta_{2} = 0.11 \times 10^{-6}$ 

Thus,

$$\delta V^i - \delta V^o = \sum_{j=0}^{i-1} \delta L^j \tag{66}$$

Similarly,  $\delta V^i - \delta V^o$  may be calculated from Eq. (64)

$$\delta V^{i} - \delta V^{o} = \left[a^{i} + V_{x}^{i} \delta x_{i} + V_{k}^{i} \delta k + \frac{1}{2} \delta x_{i}^{T} V_{xx}^{i} \delta x_{i} + \delta x_{i}^{T} V_{xk}^{i} \delta k + \frac{1}{2} \delta k^{T} V_{kk}^{i} \delta k\right] - \left[a^{o} + V_{k}^{o} \delta k + \frac{1}{2} \delta k^{T} V_{kk}^{o} \delta k\right]$$
(67)

The last equation may be simplified somewhat by noticing that  $V_{k}^{i} = V_{k}^{o}$  whenever  $\delta k$  is evaluated. Thus

$$\delta V^{i} - \delta V^{o} = a^{i} - a^{o} + V_{x^{i}} \delta x_{i} + \frac{1}{2} \delta x_{i}^{T} V_{xx^{i}} \delta x_{i} + \delta x_{i}^{T} V_{xx^{i}} \delta k + \frac{1}{2} \delta k^{T} V_{kk^{i}} \delta k - \frac{1}{2} \delta k^{T} V_{kk^{o}} \delta k$$
 (68)

and, test 2 is performed by determining whether Eq. (66) agrees with Eq. (68) within a given tolerance. If the test is failed  $\ddagger$  then  $\delta k$  should be reduced, or, if  $\delta k$  is zero,  $\delta x_i$  should be reduced by the step-size adjustment method. This test is particularly simple to apply in cases where  $L(x_i, u_i, t_i) \equiv 0$ .

## IV. Numerical Example – Comparison with McReynolds' Successive Sweep Method

## 1. Statement of the Orbit Transfer Problem

An orbit transfer problem  $^{4,5,7,12,16}$  is solved. In this problem, a control sequence must be found to maximize the radial distance of a rocket from the sun, with the terminal condition that the rocket be in a solar orbit. Here,  $x_i$  is a 3 vector, whose components represent radial distance (from the sun), radial velocity, and angular velocity, respectively, normalized so that the initial condition (in Earth's orbit) is

$$x_o = \begin{pmatrix} 1 \\ 0 \\ 1 \end{pmatrix}$$

$$\theta(x_N) = \begin{pmatrix} x_{2,N} \\ x_{3,N} - \frac{1}{(x_{1,N})_{1/2}} \end{pmatrix}$$

 $(\theta = 0)$  is the condition for a state to be in a stable orbit.)

Here,

$$\tilde{L}^i = 0, F(x_N) = x_{1,N}$$

so that

$$W = x_{1.N} + k_1 \theta_1 + k_2 \theta_2$$

$$\tilde{f}^{i} = \begin{pmatrix} x_{2,i} \\ x_{3}^{2}, i/x_{1,i} - 1/x_{1}^{2}, i + A^{i} \sin u_{i} \\ -x_{2}, x_{3,i}/x_{1,i} + A^{i} \cos u_{i} \end{pmatrix}$$

where

$$A^i = 0.1405/(1.0 - 0.07487t_i)$$

The time interval  $[0,t_N]$  is given.

Note that  $\tilde{f}^i(x_i, u_i) = \tilde{F}(x_i) + G^i(u_i)$ , so that  $\tilde{H}_{ux^i}$  and  $\tilde{f}_{ux^i}$  vanish.

This statement of the problem was inserted into Eqs. (46–54) with terms of order higher than  $\Delta t$  dropped. The relevant equations are

$$\tilde{\Delta} = \tilde{H}_{uu}{}^{i} = V_{x}{}^{i+1}G_{uu}{}^{i} \tag{69}$$

$$\beta_1 = -\tilde{\Delta}^{-1} \tilde{f}_u^{iT} V_{xx}^{i+1} \tag{70}$$

$$\beta_2 = -\tilde{\Delta}^{-1} \tilde{f}_u^{iT} V_{xk}^{i+1} \tag{71}$$

$$a^{i} = a^{i+1} + V_{x^{i+1}}[G^{i}(u_{i}^{*}) - G^{i}(\bar{u}_{i})]\Delta t$$
 (72)

$$V_{x^i} = V_{x^{i+1}} + \{V_{x^{i+1}}\tilde{F}_x(\bar{x}_i) + \}$$

$$[G^{i}(u_{i}^{*}) - G^{i}(\bar{u}_{i})]V_{xx^{i+1}}\Delta t$$
 (73)

$$V_{k^{i}} = V_{k^{i+1}} + [G^{i}(u_{i}^{*}) - G^{i}(\bar{u}_{i})]V_{xk^{i+1}}\Delta t$$
 (74)

$$V_{xk}^{i} = V_{xk}^{i+1} + [\tilde{F}_{x}(\bar{x}_{i})V_{xk}^{i+1} - \beta_{1}^{T}\tilde{\Delta}\beta_{2}]\Delta t$$
 (75)

$$V_{kk}{}^i = V_{kk}{}^{i+1} - \beta_2{}^T \widetilde{\Delta} \beta_2 \Delta t \tag{76}$$

$$V_{xx^{i}} = V_{xx^{i+1}} + \{V_{x^{i+1}}\tilde{F}_{xx}(\bar{x}_{i}) + \tilde{F}_{x}(\bar{x}_{i})^{T}V_{xx^{i+1}} + V_{xx^{i+1}}\tilde{F}_{x}(\bar{x}_{i}) + \beta_{1}^{T}\tilde{\Delta}\beta_{1}\}\Delta t \quad (77)$$

where  $u_i^*$  was found by maximizing  $\tilde{H}^i$  which was equivalent to maximizing  $V_{x^{i+1}}G^i(u_i)$ , which, in turn, was equivalent to finding the maximum of

$$V_{x,2^{i+1}}\sin u_i + V_{x,3^{i+1}}\cos u_i$$

The following necessary condition holds:

$$V_{x,2^{i+1}}\cos u_i^* - V_{x,3^{i+1}}\sin u_i^* = 0$$

<sup>‡</sup> Failure of the test at  $t_i$  ( $0 < t_i < t_N$ ) allows one to discontinue integration of this "trial trajectory" at  $t_i$  instead of integrating all the way to  $t_N$ ; this can save considerable computer time.

Table 2 400 time steps — final time =  $3.32^a$ 

t	u	$x_1$	$x_2$	$x_3$	$V_{x_1}$	$V_{x2}$	$V_{x3}$
0	0.4332	1	0	1	1.8803	0.93239	2.0340
0.166	0.5072	1.0010	0.0139	1.0200	1.7254	0.94700	1.7201
0.332	0.5937	1.0049	0.0361	1.0362	1.5729	0.93843	1.4045
0.498	0.6936	1.0132	0.0659	1.0470	1.4273	0.90323	1.0982
0.664	0.8080	1.0269	0.1020	1.0507	1.2942	0.83985	0.81261
0.830	0.9371	1.0469	0.1425	1.0464	1.1790	0.74911	0.55832
0.996	1.081	1.0740	0.1855	1.0332	1.0857	0.63411	0.34405
1.162	1.241	1.1082	0.2285	1.0114	1.0160	0.49963	0.17548
1.328	1.426	1.1493	0.2693	0.9811	0.96936	0.35134	0.054908
1.494	1.683	1.1970	0.3059	0.9428	0.94344	0.19473	-0.018536
1.660	2.645	1.2502	0.3335	0.8927	0.93488	0.034410	-0.048200
1.826	4.437	1.3048	0.3149	0.8375	0.94036	-0.12632	-0.039267
1.992	4.732	1.3542	0.2780	0.8039	0.95720	-0.28580	0.0028600
2.158	4.885	1.3972	0.2386	0.7818	0.98321	-0.44323	0.074425
2.324	4.999	1.4337	0.1988	0.7682	1.0168	-0.59804	0.17286
2.490	5.093	1.4636	0.1598	0.7617	1.0569	-0.74962	0.29642
2.656	5.176	1.4872	0.1224	0.7613	1.1029	-0.89717	0.44398
2.882	5,250	1.5047	0.0871	0.7664	1.1541	-1.0396	0.61486
2.988	5.318	1.5165	0.0546	0.7765	1.2102	-1.1755	0.80871
3.154	5.382	1.5232	0.0254	0.7910	1.2709	-1.3029	1.0253
3.320		1.5254	0.0000	0.8097	1.3356	-1.4194	1.2646

 $^{a}V = 1.52537493, k_{1} = -1.41936325, k_{2} = 1.26460750, \theta_{1} = -0.33 \times 10^{-6}, \theta_{2} = 0.37 \times 10^{-7}.$ 

whence,

$$u_i^* = \arctan(V_{x,2}^{i+1}/V_{x,3}^{i+1}) \tag{78}$$

Terms of higher order in  $\Delta t$  were dropped on the assumption that such terms were negligible in comparison with those of order  $\Delta t$ .

In the forward integration phases,  $u_i = u_i^* + \delta u_i$  was computed directly by maximizing

$$\tilde{H}^{i}(\bar{x}_{i} + \delta x_{i}, u_{i}, V_{x^{i+1}} + \delta x_{i+1}^{T} V_{xx^{i+1}} + \delta k^{T} V_{kx^{i+1}}) =$$

$$(V_{x^{i+1}} + \delta x_{i+1}^{T} V_{xx^{i+1}} + \delta k^{T} V_{kx^{i+1}}) [\tilde{F}(\bar{x}_{i} + \delta x_{i}) + G^{i}(u_{i})] \quad (79)$$

with respect to  $u_i$ . Note that  $\delta x_{i+1}$  should be replaced by Eq. (14), which for this problem becomes

$$\delta x_{i+1} = \delta x_i + \Delta t \{ [G^i(u_i) - G^i(\bar{u}_i)] + \tilde{F}_x(\bar{x}_i)\delta x_i + \frac{1}{2}\delta x_i^T \tilde{F}_{xx}(\bar{x}_i)\delta x_i \}$$
(80)

However, this is of higher order than the degree of approximation, and it is satisfactory to replace  $\delta x_{i+1}$  in Eq. (79) by  $\delta x_i$ .

The new criteria described in the previous section were experimentally applied. Test 1 appeared to be essential for the algorithm to converge. Without it,  $\delta k$  was often chosen too large. Test 2 was found to be helpful and time saving. A more detailed discussion is given in Sec. V.

#### 2. Comparison with Successive Sweep Method

Our algorithm converges somewhat faster than McReynolds' Successive Sweep Method<sup>4-6</sup> on this problem, starting from the same initial nominal solution. This may be because the two techniques differ primarily in the minimization,\(^8\) and the  $f^i - \bar{f}^i$  and  $H^i - \bar{H}^i$  terms which are present here, but are absent from the Successive Sweep Method. However, close to the optimal, these terms are small, so that our minimization yields results which are close to McReynolds'. Thus, close to the optimal, the algorithms are very nearly the same. Earlier in the computation, the terms are large, and the minimization permits the present routine to take larger steps. Thus, this routine is able to reach the vicinity of the optimal in fewer iterations than the Successive Sweep Method,

and once there, takes just as many additional iterations to converge.

Note that this routine does not evaluate  $H_{uu}$  (or  $\Delta$ ) until after a minimization has been performed, so that  $H_{uu}$  is negative (definite). McReynolds evaluates  $H_{uu}$  on the nominal trajectory, and so he must either choose his initial nominal so that  $H_{uu}$  is negative, or he must invoke a device to partially overcome the difficulty.

#### V. Numerical Results

#### 1. Discussion of the Trajectories in Tables 1-4

Tables 1–3 list optimal trajectories calculated for the orbittransfer problem obtained by means of the algorithm described previously.

The value of 3.32 was used for  $t_N$  in order to compare results with those described in Refs. 4 and 5. The other value, 3.3194, was determined in Ref. 16, where the authors solved a minimum time problem. Their problem was identical with the present problem, except that they specified  $x_1(t_N) = 1.525$  (corresponding to the orbit of Mars) as a constraint and left  $t_N$  free. Our results agree most closely with those of Ref. 16. (The normalized values of  $V_{x^0}$  agree with  $\lambda(t_0)$  given in Ref. 16 to 3 figures.)

The rather large differences between the results of 100 time steps and of 400 steps indicate that 100 "Euler integration" steps are not really sufficient to model the continuous time dynamic system.

Table 4 contains a trajectory which maximizes W without regard to terminal constraints for nearly optimal values of  $k_1$  and  $k_2$ . It is interesting to note that the maximum obtained for W is far from the maximum W obtained in Tables 1-3, and  $\theta$  is not zero. Thus the free-end point problem, with  $k_1$  and  $k_2$  set to their optimal values, has at least two local maxima; the one maximum coincides with the point  $\theta = 0$ , while the other does not. (We have found that if, starting with this other maximum solution and the optimal k's, the k's are changed successively to reduce  $|\theta|$ , the optimal solution to the problem is obtained, i.e., the k's are adjusted away from their "optimal" values, but again return to these optimal values, at which stage the "correct" minimum of W is attained and  $\theta = 0$ .)

On the average, the program took approximately  $3 \sec$  per iteration for the 100-step program and  $12 \sec$  per iteration

<sup>§</sup> Which becomes a maximization in this problem.

 $<sup>\</sup>P - |H_{uu}^i + B^i|$  is used in place of  $H_{uu}^i$  where  $B^i$  is chosen to go to zero as the nominal is approached.

Table 3 400 time steps — final time =  $3.3194^a$ 

t	u	$x_1$	$x_2$	$x_3$	${V}_{x_1}$	${V}_{x_2}$	$V_{x_3}$
0	0.4333	1	0	1	1.8800	0.93244	2.0334
0.166	0.5074	1.0010	0.0139	1.0199	1.7252	0.94699	1.7196
0.332	0.5938	1.0049	0.0361	1.0362	1.5727	0.93838	1.4041
0.498	0.6937	1.0131	0.0658	1.0470	1.4272	0.90314	1.0979
0.664	0.8080	1.0268	0.1019	1.0507	1.2941	0.83974	0.81232
0.830	0.9372	1.0469	0.1425	1.0464	1.1790	0.74899	0.55811
0.996	1.081	1.0739	0.1854	1.0332	1.0856	0.63399	0.34391
1.162	1.242	1.1081	0.2284	1.0114	1.0160	0.49953	0.17540
1.328	1.426	1.1493	0.2692	0.9812	0.96934	0.35127	0.054860
1.494	1.683	1.1969	0.3059	0.9429	0.94343	0.19468	-0.018561
1.660	2.645	1.2501	0.3334	0.8927	0.93487	0.034386	-0.048213
1.826	4.437	1.3046	0.3148	0.8375	0.94035	-0.12631	-0.039278
1.992	4.732	1.3540	0.2779	0.8040	0.95720	-0.28576	0.002844
2.158	4.885	1.3971	0.2386	0.7819	0.98321	-0.44317	0.074400
2.324	4.999	1.4335	0.1988	0.7682	1.0168	-0.59796	0.17282
2.490	5.093	1.4634	0.1598	0.7617	1.0569	-0.74951	0.29636
2.656	5.176	1.4870	0.1223	0.7614	1.1029	-0.89703	0.44390
2.821	5.250	1.5045	0.0871	0.7665	1.1541	-1.0394	0.61476
2.987	5.318	1.5163	0.0546	0.7765	1.2103	-1.1753	0.80858
3.153	5.382	1.5230	0.0254	0.7911	1.2709	-1.3026	1.0252
3.319		1.5252	0.0000	0.8097	1.3357	-1.4191	1.2644

 $<sup>^{\</sup>circ}V = 1.52516085, k_1 = -1.41910912, k_2 = 1.26441935, \theta_1 = -0.10 \times 10^{-5}, \theta_2 = -0.26 \times 10^{-6}.$ 

for the 400-step program on an IBM 7094 computer. For this purpose, the "number of iterations" is defined as the number of times Eqs. (27, 28, and 32) were integrated. Thus an iteration includes at least one but possibly as many as 9 integrations of the state Eqs. (1). Also, an iteration may include the integration of Eqs. (30) and (31) and calculation of  $\delta k$  by Eq. (59). In the earlier versions of the program, where test 2 was absent, iteration times averaged as much as 6 sec for 100-step trajectories. More details on this follow.

The nominal used to compute the trajectory in Table 1 was the nominal McReynolds used:  $\bar{k}_1 = -1$ ;  $\bar{k}_2 = 1$ ;  $\bar{u}(t) = 1.57078$  for  $0 \le t \le 1.66$ ;  $\bar{u}(t) = 5.7124$  for 1.66 < t < 3.32. Convergence to  $|\theta_i(x_N)| < 10^{-6}$  (i = 1,2) required 15 iterations.

The nominal used for Tables 2 and 3 is the optimal control computed in Ref. 5. (This was linearly interpolated to 100 points, and then expanded to 400 points by repeating each value four times.) For Table 2,  $\bar{k}_1 = -1.41936541$ ,  $\bar{k}_2 = 1.264609$ , and convergence required 10 iterations. For

Table 3,  $\bar{k}_1 = -1.399631$ ,  $\bar{k}_2 = 1.260031$  (optimal values from<sup>4</sup>), and 11 iterations were required.

Starting conditions for Table  $\hat{4}$  are the nominal control used in Table 1, and the values of  $\bar{k}_1$  and  $\bar{k}_2$  used in Table 3. "Convergence" required 6 iterations.

#### 2. Use of Tests 1 and 2

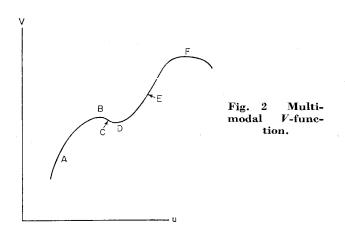
With neither test 1 nor test 2 present, the algorithm did not converge. Constraining each new trajectory by the requirement that test 1 be satisfied was sufficient to ensure convergence. Because this constraint was usually effective—i.e., many values of  $\delta k$  were rejected—this problem appears to be very sensitive to changes in the multipliers k.

Two programs were compared; one used only test 1, the other used both tests. The comparison indicates a certain redundancy between the two tests. A large number of trial  $\delta k$ 's were rejected by both test 1 (where that was the only test) and test 2 (where both tests were used.) In fact, the same values of  $\delta k$  were ultimately accepted by the two pro-

Table 4 100 time steps — final time =  $3.32^a$ 

t	u	$x_1$	$x_2$	$x_3$	$V_{x_1}$	$\overline{V}_{x_2}$	$V_{x3}$
0	1.147	1	0	1	1.5399	3.8503	1.5607
0.166	1.458	1.0015	0.0233	1.0055			
0.332	1.802	1.0071	0.0489	0.9993	0.065221	3.4865	-1.1789
0.498	2.172	1.0167	0.0706	0.9812			
0.664	2.423	1.0294	0.0826	0.9529	-1.2528	2.6667	-3.5848
0.830	2.674	1.0433	0.0833	0.9200			
0.996	2.819	1.0565	0.0722	0.8850	-2.0365	1.7928	-5.1481
1.162	2.917	1.0672	0.0508	0.8525			
1.328	2.990	1.0738	0.0203	0.8221	-2.4128	1.0467	-5.9689
1.494	3.048	1.0747	-0.0184	0.7956			
1.660	3.098	1.0686	-0.0650	0.7737	-2.6385	0.39794	-6.2592
1.826	3.143	1.0543	-0.1194	0.7572			
1.992	3.186	1.0305	-0.1818	0.7472	-2.7998	-0.14885	-6.0700
2.158	3.229	0.9957	-0.2532	0.7452			
2.324	3.275	0.9484	-0.3349	0.7536	-2.9268	-0.59906	-5.3983
2.490	3.331	0.8867	-0.4294	0.7765			
2.656	3.406	0.8083	-0.5404	0.8211	-2.9898	-0.97790	-4.1832
2.822	3.528	0.7100	-0.6738	0.9021			
2.988	3.778	0.5878	-0.8374	1.0534	-2.6070	-1.3288	-2.2274
3.154	4.473	0.4361	-1.0316	1.3731			
3.320		0.2559	-1.0621	2.2275	5.8682	-1.3996	1.2600

 $<sup>^{</sup>a}V = 2.05800182, k_{1} = -1.3996310, k_{2} = 1.2600310, \theta_{1} = -1.0620840, \theta_{2} = 0.25048833.$ 



grams, and the programs generally converged to the same optimal trajectory in the same number of steps. However, the redundancy was not complete; there were  $\delta k$ 's that were accepted by test 2 and rejected by test 1.

Note that this redundancy is helpful. Test 2 can be invoked often in the forward integration phare, whereas test 1 can only be invoked after the forward integration phase is complete. Thus test 2 can save execution time. This time appears to be quite significant: with both tests present, a 100-step iteration took about 3 sec. With only test 1, a 100-step iteration took, on the average, more than 6 sec. (The forward integration of the system equations can be terminated as soon as test 2 fails. However, test 1 requires that the integration be performed up until  $t_N$ . This accounts for the "time saving" when test 2 is included.)

A difficulty was encountered in using the tests. As the algorithm approached the optimal, steps and changes in parameters became small. Tests 1 and 2, which involve differences of large quantities, became less reliable—in fact, excessively conservative. In order to overcome this difficulty, test 1 was disabled when  $\delta V^o = V^o - \overline{W}^o$  was less, in absolute value, than  $10^{-6}\overline{W}^o$ , and test 2 was disabled when the absolute value of

$$a^o + V_{k^o} \delta k + \frac{1}{2} \delta k^T V_{kk^o} \delta k$$

was less than  $10^{-6}\overline{W}^{o}$ .

#### 3. Behavior of the Algorithm

The existence of the maximum in Table 4 may be illustrated by analogy with a static maximization of a function of a single variable. (See Fig. 2.)

In order to maximize V(u), one may approximate V with a second-order Taylor expansion in the neighborhood of  $\bar{u}$ , a nominal value;

$$V(u) \approx V(\bar{u}) + V'(\bar{u})(u - \bar{u}) + \frac{1}{2}V''(\bar{u})(u - \bar{u})^2$$
 (81)

The value of u that maximizes this is given by

$$0 = V'(\bar{u}) + V''(\bar{u})(u - \bar{u})$$

or

$$u = \bar{u} - V'(\bar{u})/V''(\bar{u}) \tag{82}$$

Equation (81) may be used to predict the improvement in V using Eq. (82). The improvement is

$$V(u) - V(\bar{u}) = -\frac{1}{2} V'(\bar{u})^2 / V''(\bar{u})$$
 (83)

which is positive for V''(u) < 0.

If  $\bar{u}$  is at point A, and the local maximum at point B is the one desired (rather than the one at point F), some means must be employed to guarantee that Eq. (82) will produce a value of u in the neighborhood of B. A value near E will eventually converge to F. Thus, Eq. (82) should be re-

placed by

$$u = \bar{u} - \epsilon V'(\bar{u})/V''(\bar{u}) \tag{84}$$

Then, Eq. (83) becomes

$$V(u) - V(\bar{u}) = (\frac{1}{2}\epsilon^2 - \epsilon)V'(\bar{u})^2/V''(\bar{u})$$
 (85)

Thus an improvement is guaranteed at every stage if Eq. (84) is used with proper choice of  $\epsilon$ , and if the initial nominal lies somewhere to the left of point D. If the nominal is to the right of point E, the algorithm will tend to point F. Points between C and E are problematical because V''(u) is not negative-definite.\*\* In neighborhoods of C and E, Eqs. (84) and (85) are not useable.

The aforementioned "Newton-Raphson" algorithm is not perfectly analogous to the algorithm for discrete-time dynamic optimization algorithms, but some comparisons can be drawn. In the discrete dynamic case, u may be thought of as an N-vector (N = 100 or 400). Then V' is a vector, V'' is a matrix, and  $\epsilon$  represents the step-size adjustment method. Figure 1 may be thought of as a graph of V as a function of u for constant, near optimal k. Point B is the local maximum where  $\theta_1 = \theta_2 = 0$  (Tables 1–3). Point F is the maximum of Table 4.

Behavior due to a point analogous to E has been observed. Iteration began at point A, for near optimal k. The next value of u was to the right of point D (because V calculated at that point was greater than that of Table 1. In this case,  $N = 100, t_{\rm N} = 3.32$ ). In successive iterations, V continued to increase, as did  $|\theta_1|$  and  $|\theta_2|$  because u was chosen to maximize H. However, it was impossible to drive  $a^{o}$  [analogous to (85)] below a certain value. After a few iterations, a<sup>o</sup> began to increase. Finally,  $a^{o}$  jumped from a typical value of less than  $10^{-8}$  to more than 300 in one iteration. At that iteration, elements of  $V_{xx}$  were of the order of 5000. This situation corresponds to a point near C or E where  $V_{uu}$  is near singular (the singularity manifests itself in the large values of  $V_{xx}$  and  $a^{\circ}$ ). Thus, in order to guarantee proper convergence, iterations must be restricted to the neighborhood of the relative minimum desired. In the present algorithm, the restrictions are accomplished by 1) the choice of a "sufficiently good" nominal, 2) minimization of H(u) (rather than the use of  $\delta u = -H_{uu}^{-1}H_u$  as in Refs. 5, 6, 8, and 11), 3) test 2.

### VI. Conclusion

A new discrete algorithm has been derived which is analogous to the continuous algorithms of Refs. 1 and 2. Extensions to the latter (test 1 and test 2) have been developed to ensure that the new iteration is in the neighborhood of the current nominal. The algorithm has been used to solve a nonlinear, optimal orbit transfer problem. This problem has been attempted, and solved, in various forms, by a number of investigators using different computational methods. The numerical results obtained in this paper agree most closely with those of Ref. 16.

A more detailed description of the numerical solution of the optimal orbit transfer problem is given in Ref. 17. Tables of the second-partial-derivatives of V are given, and the optimal feedback gains are listed.

# Appendix A: Continuous Results from Jacobson

The following is a statement and solution of the continuous-time optimal control problem solved in Refs. 1 and 2. The notation has been modified to conform to that of this paper. Thus some expressions involving derivatives

<sup>\*\*</sup> In the case of vector u, an increased cost may be obtained even if V''(u) is non-negative-definite. In the scalar case this is not possible.

have been transposed, and  $\sim$  has been placed over certain symbols to coincide with Sec. III.1.

Given that

$$\dot{x} = \tilde{f}(x, u, t); \quad x(t_0) = x_0$$
 (A1)

Find u(t),  $t \in [t_o, t_f]$  to minimize

$$\hat{W}(x_0, t_0) = \int_{t_0}^{t_f} \tilde{L}(x, u, t) dt + F[x(t_f)]$$
 (A2)

while satisfying

$$\theta[x(t_f)] = 0 \tag{A3}$$

The constraints (A3) are adjoined to the cost functional (A2):

$$W(x_0, k, t_0) = \hat{W} + k^T \theta [x(t_f)]$$
 (A4)

The relevant equations are

$$\beta_1 = -\tilde{H}_{uu}^{-1}(\tilde{H}_{ux} + \tilde{f}_u^T V_{xx}) \tag{A5}$$

$$\beta_2 = -\tilde{H}_{uu}^{-1} \tilde{f}_u^T V_{xk} \tag{A6}$$

$$-\dot{a} = \tilde{H} - \bar{\tilde{H}} \tag{A7}$$

$$-\dot{V}_x = \tilde{H}_x + (\tilde{f} - \bar{\tilde{f}})V_{xx} \tag{A8}$$

$$-\dot{V}_k = (\tilde{f} - \tilde{\tilde{f}})V_{xk} \tag{A9}$$

$$-\dot{V}_{xk} = (\tilde{f}_{x}^{T} + \beta_{1}^{T} \tilde{f}_{u}^{T}) V_{xk}$$
 (A10)

$$-\dot{V}_{kk} = -V_{xk}^{T} \tilde{f}_{u} \tilde{H}_{uu}^{-1} \tilde{f}_{u}^{T} V_{xk} \tag{A11}$$

$$-\dot{V}_{xx} = \tilde{H}_{xx} + \tilde{f}_{x}^{T}V_{xx} + V_{xx}\tilde{f}_{x} -$$

$$(\tilde{H}_{ux} + f_u^T V_{xx})^T \tilde{H}_{uu}^{-1} (H_{ux} + f_u^T V_{xx})$$
 (A12)

where  $\tilde{H} = \tilde{L} + V_x \tilde{f}$ , and derivatives of H are taken with  $V_x$  constant, i.e.,

$$\tilde{H}_x = \tilde{L}_x + V_x \tilde{f}_x$$

The boundary conditions for Eqs. (A7-A12) are the same as Eqs. (33-38).

### Appendix B: Step-Size Adjustment Method

In the first stage of the algorithm (Sec. III.2) k is kept constant. Then Eq. (22), the linear feedback law, becomes

$$\delta u_i = \beta_i \delta x_i \tag{B1}$$

and the perturbed state Eq. (1) becomes

$$\bar{x}_{i+1} + \delta x_{i+1} = f(\bar{x}_i + \delta x_i, u_i^* + \beta_1 \delta x_i t_i)$$
 (B2)

with

$$\bar{x}(t_0) + \delta x(t_0) = x_0$$

Since  $\delta x(t_o) = 0$ ,  $\delta x_i$  produced by Eq. (B2) is due to the driving action of  $\delta u_i^* = u^*_i - \bar{u}_i$ .

The size of  $\delta x_i$  can be restrained by altering the time interval over which Eq. (B2) is evaluated. Consider the time interval  $[t_{N_1}, t_N]$  where  $0 \le N_1 < N$ . Assume one runs along the nominal trajectory  $\bar{x}_i$  from  $t_o$  to  $t_{N_1}$ . At time  $t_i =$  $t_{N_1}, x(t_{N_1}) = \bar{x}(x_{N_1})$  since the path of the nominal trajectory has been followed from  $t_o$  to  $t_{N_1}$  (i.e.,  $\delta x_i$ ;  $i \in [0, N_1]$  is zero). Now consider integrating (B2) over the interval  $[t_{N_1}, t_N]$ . If  $[t_{N_1},t_N]$  is small, then  $\delta x_i$  produced by (B2) in this interval will be small, even for large  $\delta u_i^*$ , since there are very few steps over which to sum (B2) with initial conditions

$$\delta x(t_{N_1}) = 0$$

By making  $N_1$  near  $N_i$ , one can generally force  $\delta x_i$  to be sufficiently small.

This description is summarized in the following statement. There exists a time  $t_{N_1}$ , sufficiently close to  $t_N$ , in the range  $t_o \leq t_{N_1} < t_N$ , such that if the nominal trajectory is followed from  $t_0$  to  $t_{N_1}$  and then (B2) is integrated from  $t_{N_1}$  to  $t_N$ ,  $\delta x_i$ , in the interval  $[t_{N_1}, t_N]$  will be small enough for the second-order expansions of V, L, and f to be valid.

The following questions must be answered. 1) How does one decide if  $\delta x_i$  is "small enough?" 2) How does one chose  $N_1$  such that  $\delta x_i$  is "small enough?"

The answers are: 1) From Eq. (27),

$$\left| a^{N_1} \right| = \left| \sum_{i=N_1}^{N-1} H^i - \tilde{H}^i + \frac{1}{2} (f^i - \tilde{f}^i)^T V_{xx} (f^i - \tilde{f}^i) \right|$$

is the predicted improvement in cost when starting at the

point  $\bar{x}_{N_1}$  and using  $u_i = u_i^* + \beta_1 \delta x_i$ . Assume for the moment that  $N_1 = 0$ . Integrate Eq. (B2) and calculate the cost W. The actual improvement in

$$\Delta V = \overline{W}(\bar{x}_0, \overline{k}, t_0) - W(\bar{x}_0, \overline{k}, t_0)$$
 (B3)

If this actual improvement in cost is "near" to the predicted value  $|a^{N_1}|$  then  $\delta x_i$ , produced by the new control acting through Eq. (B2), is considered "small enough."

It is convenient in practice to define "near" in the following way. If the following inequality is satisfied,  $\Delta V$  is considered to be "near"  $|a^{N_1}|$ :

$$\Delta V/|a^{N_1}| > c; \quad c \ge 0 \tag{B4}$$

In practice c is set as 0.5. There are no hard and fast rules for setting c. Certainly it should be greater than or equal to zero since a negative  $\Delta V$  is inadmissible. c should not be greater than unity since one should not expect improvement in cost greater than predicted, if the expansions for V, L and f are valid. Moreover, c should be somewhat less than unity so that any decisions based on Eq. (B4) are not influenced by round-off errors in the computations.

A more precise criterion which is relevant here is test 2, described in Sec. III.4. Test 2 was used in addition to Eq. (B4) in the program that produced Tables 1-4.

2) If test (B4) is passed with  $N_1 = 0$ , all is well, and the next iteration of the main algorithms may be begun with the knowledge that a reasonable reduction in cost of  $\Delta V$  has been made. If (B4) is not satisfied, then set

$$N_1 = N/2 = N_{o1} (B5)$$

The aforementioned procedure is repeated with this  $N_1$  and Eq. (B4) is checked again (with the new  $\Delta V$ ). If it is satisfied, then the next iteration is begun. If not, then set

$$N_1 = (N - N_{o1})/2 + N_{o1} = N_{o2}$$
 (B6)

and repeat again.

In general

$$N_1 = (N - N_{or})/2 + N_{or} = N_{or+1}$$
 (B7)

where  $r = 0,1 \dots$  and  $N_{oo} = -N$ .

It may happen that the nominal trajectory  $\bar{x}_i$  is optimal in an interval  $[N_2,N]$ ;  $N_2 \in [0,N]$ , but is nonoptimal in the interval [0,N]. If  $N_1$  is being found in the manner outlined above, then some  $N_{or}$  may fall in the interval  $[N_2,N]$ . Then  $\delta x_i$  in the interval  $[N_1, N]$  would be zero because  $u_i^* = \bar{u}_i$ ;  $i \in [N_2, N]$ , so that no reduction  $\Delta V$  in cost would occur, even though the whole trajectory  $\bar{x}_i$  is nonoptimal in [0,N]. One must insure, therefore, that  $N_1$  will never fall in  $[N_2,N]$ .

This is accomplished easily in the following way. From Eq. (33),  $a^N=0$ . When integrating the backwards equations monitor  $|a^i|$ . Record the step  $N_{eff}$  when  $|a^i|$  becomes different from zero. (Or in practice, when it becomes greater than a small, positive quantity,  $\eta$ .) The trajectory between  $N_{eff}$  and N satisfies a necessary condition of optimality, viz.,

$$a^i = 0, i = N_{eff}, \dots, N$$
 (B8)

If, on the forwards run, a time  $N_1 \neq 0$  must be found, then the time interval  $[0,N_{eff}]$  is subdivided as described earlier, and not [0,N]. As the over-all trajectory becomes more and more optimal, from iteration to iteration, so  $N_{eff} \rightarrow 0$ . Finally, on an optimal trajectory,  $|a^i| < \eta$ ;  $i = 0, \ldots, N$  and  $N_{eff} = 0$  and the computation is stopped.

Thus, Eq. (B7) becomes

$$N_1 = (N_{eff} - N_{or})/2 + N_{or} = N_{or+1}$$
 (B9)

where  $N_{\infty} = 2 - N_{eff}$  and r = 0,1... Integer division is used in (B7) and (B9) and r is increased until  $N_1 = N_{eff} - 1$ . If  $N_{eff} = 1$  then only r = 0 is used.

It should be appreciated that since there are a finite number N-1 of discrete time steps, this subdivision can only be done a finite number of times. For problems like those of Section III.1, the smallest possible nonzero time interval is  $\Delta t = (t_f - t_o)/(N-1)$ . It is clear that N must be large enough such that  $\delta x_i$  produced during this basic interval is "small enough." This restriction is a practical one, brought about by the discrete time nature of the digital computation.

When  $\Delta V$  and  $|a^{N_1}|$  are small, but  $> \eta$ , the criterion (B4) may be too severe with c=0.5, owing to round-off errors. There may thus come a stage where (B4) remains unsatisfied even when  $N_1=N_{eff}-1$ . If this happens, set c=0.0 and repeat the procedure for determining  $N_1$ . c=0 is a much less stringent test because it asks only that  $\Delta V>0$ . If once again (B4) is unsatisfied, even when  $N_1=N_{eff}-1$ , then stop the computation since no further reduction in cost is possible. This implies that either optimality has been attained (in which case  $|a^o| < \eta$  and so  $N_{eff} < 1$ ) or N is not large enough and hence  $\Delta t$  is too large a basic time interval. For additional refinements of the step-size adjustment method see Ref. 1, Chap. 4.

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